

Adam KONIUSZY  
Piotr KOSTENCKI  
Andrew BERGER  
Wojciech GOLIMOWSKI

## POWER PERFORMANCE OF FARM TRACTOR IN FIELD OPERATIONS

### WYKORZYSTANIE MOCY CIĄGNIKA ROLNICZEGO W PRACACH POŁOWYCH

*Many studies have examined the effects of agriculture tractor engine energy performance. This paper presents an evaluation method of such engine actual power use during plowing operations. It includes results of a comparative study of power performance of a 230 kW tractor model John Deere 8330 subject to soil plowing operations as a function of field size: A (26 ha), B (12.74 ha), C (3.22 ha). Statistical data clustering, a relatively novel approach in studies on actual utilization of engine power, was used. A positive correlation was observed between field size and the active state of the engine: 75.2% field A; 68.8% field B; 46.8% field C. The actual power utilization of agriculture tractor engine as a function of field size was 0.62, 0.58 and 0.39 respectively for the three fields used in this study. With this evaluation approach, performance indexes of operational power performance in various conditions were obtained for possible use in optimization of plowing operations.*

**Keywords:** agriculture tractor, plowing, power performance, engine operation clusters.

*Ocena stanu obciążenia silnika spalinowego w pojeździe podczas eksploatacji jest przedmiotem wielu prac badawczych. W artykule przedstawiono nową metodę oceny wykorzystania mocy silnika ciągnika rolniczego eksploatowanego podczas orki. Zaprezentowano wyniki badań porównawczych nad wykorzystaniem mocy ciągnika John Deere 8330 (230 kW) w odniesieniu do powierzchni uprawianych pól: A (26 ha), B (12,74 ha) i C (3,22 ha). Do analizy danych pomiarowych zastosowano po raz pierwszy statystyczną metodę grupowania punktów pomiarowych. Na podstawie wyników badań stwierdzono silną korelację dodatnią pomiędzy powierzchnią pól a stanem obciążenia silnika: 75,2% pole A; 68,8% pole B; 46,8% pole C. Opracowany wskaźnik efektywnego wykorzystania mocy silnika ciągnika rolniczego wyniósł odpowiednio: 0,62, 0,58 i 0,39. Stwierdzono, że uzyskane wartości wskaźnika efektywności wykorzystania mocy silnika mogą być przydatne do optymalizacji pracy ciągnika w pracach polowych.*

**Słowa kluczowe:** ciągnik rolniczy, orka, wykorzystanie mocy, czas pracy silnika.

#### 1. Introduction

Tractors play a fundamental role in agriculture as the main power resource for operation with various add-on agriculture machinery. The most energy and labor intensive among agro-technological operations is soil plowing. The trend in a plow design favors tractors with substantial power [24, 26], but ultimately it is determined by the size and construction of the machinery satisfying the needs of smaller farms [19].

Optimal tractor and machinery parameter selection, as a function of various field operations, not only improves the economics of such activities, but also reduces exhaust pollution and other negative environmental effects. The power requirements and energy consumption may be reduced through optimizing power characteristics and engine parameters [2, 3, 11, 31].

The CO<sub>2</sub> emissions may be reduced by minimizing idling states of the engine and maximizing the engine work load. The operational engine parameters are engine speed, transmission gear ratios and engine torque [1, 14]. The experience and reaction time of the tractor operator also play an important role in maintaining these parameters in optimal range [4, 18, 23, 28, 29] and optimal engine utilization [4, 12, 21].

Monitoring the performance indexes of operational power in various conditions provides data of engine modes of operation and fuel consumption. Not many methods and mathemati-

cal power performance models as a function of field parameters exist.

In this paper we present our evaluation method and introduce the performance indexes of operational power performance obtained in various conditions. It includes the evaluation of power use of an agriculture tractor engine in various plowing operations and the results of a comparative study of power performance as a function of field size. Other studies [9, 10, 20] focus more on fuel and energy consumption efficiency and toxic exhaust emission characteristics.

#### 2. Methodology

The study took place during the 2012 plowing season on the Agrofirma agricultural farm (Witkowo, Poland) for rapeseed sowing. The experimental setup included three fields (Fig. 1). The physical parameters of the three fields' soils were measured at the time of the plowing operations and are included in Table 1 [17].

This paper presents a comparative study of power performance of a 230 kW tractor model John Deere 8330 subject to soil plowing operations on the three fields. The tractor was pulling a Lemken semi-mounted reversible, full moldboard 7-furrows EuroDiamant plow unit combined with a Campbell soil compaction roller tiller. All operations involved the same one tractor operator reducing any comparative discrepancy in experiment results.

Table 1. Soil Parameters

Soil		Soil Layer	Field					
			A		B		C	
Soil Granulation, %	2 ≥ d > 1	Tillage Layer	2.7	LFS	1.5	FSL	1.7	FSL
	1 ≥ d > 0.5		7.9		6.2		6.4	
	0.5 ≥ d > 0.25		15.1		11.0		12.5	
	0.25 ≥ d > 0.1		33.2		31.6		31.1	
	0.1 ≥ d > 0.05		17.1		17.7		19.3	
	0.05 ≥ d > 0.02		8		14		10	
	0.02 ≥ d > 0.002		11		13		14	
	d ≤ 0.002		5		5		5	
Soil Organic Matter Content, %			2.1		1.9		2.0	
Soil Moisture (by weight), %		0 - 10 cm	15.0 s=2.0		13.7 s=1.0		13.3 s=1.3	
		10 - 20 cm	15.0 s=2.3		13.5 s=0.5		13.9 s=1.2	
		20 - 30 cm	14.3 s=2.0		13.1 s=0.3		13.9 s=1.9	
Soil Volume Density, g/cm <sup>3</sup>		0 - 10 cm	1.35 s=0.10		1.31 s=0.15		1.44 s=0.15	
		10 - 20 cm	1.57 s=0.14		1.57 s=0.04		1.62 s=0.06	
		20 - 30 cm	1.57 s=0.10		1.52 s=0.03		1.65 s=0.07	
Soil Compactness, kPa		0 - 10 cm	538 s=258		535 s=192		758 s=439	
		10 - 20 cm	1183 s=463		1539 s=348		2459 s=683	
		20 - 30 cm	2212 s=588		2423 s=533		3257 s=373	
Soil Shear Stress, kPa		0 - 10 cm	24 s=10		18 s=6		18 s=4	
		10 - 20 cm	50 s=16		35 s=6		49 s=19	
		20 - 30 cm	56 s=11		53 s=10		67 s=15	
Plow Operation Velocity, m/s			2.53 s=0.23		2.58 s=0.46		2.61 s=0.48	
Operating Plow Depth, cm			25 s=2		22 s=2		25 s=3	
Operating Plow Width, m			3.34 s=0.05		3.36 s=0.04		3.27 s=0.03	

LFS - loamy fine sand, FSL - fine sandy loam, s-standard deviation, d - particle size

uring system [7]. The readings were used to calculate nominal and operational power of the engine. There are many methods of finding engine torque  $M_o$  indirectly [5, 8, 16, 22, 27, 32-34]. In our study, a method patented by the West Pomeranian University of Technology in Szczecin was utilized. In our view this method is unique and quite suitable for practical use in field operations [15, 16]. Other known methods focus more on theoretical analysis or represent laboratory experimental findings. In this study, the engine torque  $M_o$  parameter was evaluated indirectly based on the measurement of fuel consumption and engine crankshaft rotations:

$$M_o = a \cdot g_{1000}^3 + b \cdot g_{1000}^2 + c \cdot g_{1000} + d, (1)$$

where:

$$g_{1000} = \frac{V_{fuel}}{n_s} \cdot 1000, (2)$$

- $M_o$  – engine torque in Nm,
- $g_{1000}$  – fuel consumption in dm<sup>3</sup> per 1000 crankshaft revolutions,
- $a, b, c, d$  – coefficients subject to the engine type and rpm (Table 2),
- $V_{fuel}$  – fuel consumption, dm<sup>3</sup>/min,
- $n_s$  – engine speed, rpm.

The values of torque were obtained indirectly with appropriate coefficient units to satisfy equation (2).

Engine utilization was evaluated with:

$$E_N = \frac{N_u}{N_{nom}} \cdot \frac{U_t}{100\%}, (3)$$

where:

- $E_N$  – engine utilization,
- $N_u$  – plowing operation engine power, kW,
- $N_{nom}$  – nominal engine power, kW,
- $U_t$  – engine plowing operation time in relation to total engine operation time, %.

Table 2. Engine coefficients  $a, b, c, d$  – dyno test bench verified [16]

Engine speed range $n_s$ , rpm	Coefficient values			
	$a$ , Nm/dm <sup>9</sup>	$b$ , Nm/dm <sup>6</sup>	$c$ , Nm/dm <sup>3</sup>	$d$ , Nm
< 950	-7·10 <sup>-6</sup>	0.0042	1.3992	-1.1506
950-1250	-6·10 <sup>-6</sup>	0.0040	1.3193	14.087
1250-1550	-8·10 <sup>-6</sup>	0.0063	0.8354	37.374
1550-1850	-1·10 <sup>-5</sup>	0.0070	0.9304	20.479
1850-2150	-1·10 <sup>-5</sup>	0.0094	0.3923	50.361
> 2150	-7·10 <sup>-6</sup>	0.0068	0.5357	59.126

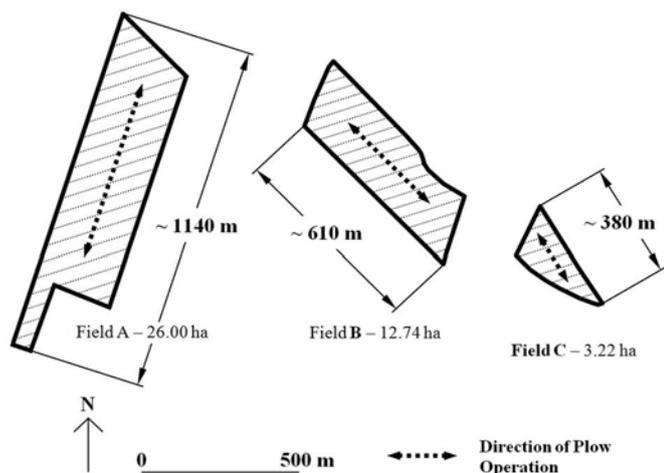


Fig. 1. Experimental Setup of three fields (based on Agrofirma geographical map)

## 2. Analysis method

The operational parameters (the engine speed, torque and power, fuel consumption and GPS position) were monitored with digital sensors with 1 Hz frequency using Siemens VDO -EDM 1404.01 meas-

The engine actual torque values were obtained from (1) and (2).

The measurements of relative time of engine operation are presented in Fig. 2, 3, 4 relative to total time of engine operation [6] and based on (4):

$$TD_{(i,j)} = \frac{t_{(i,j)}}{t_c} \cdot 100\% , \quad (4)$$

where:

$TD_{(i,j)}$  – Relative time of engine operation (Time Density), %,

$i$  – Index of the engine speed coordinate with  $\Delta n_s = 100$  rpm,

$j$  – Index of the engine torque with  $\Delta M_o = 50$  Nm,

$t_{(i,j)}$  – time of operation at  $(i, j)$ ,

$t_c$  – total time of engine operation.

Since the comparison and interpretation of the  $TD$  distribution plots (Fig. 2, 3, 4) may not be straightforward, a statistical data clustering (*k-means full binding*) method was used to obtain parameters for better quantitative comparison of effective utilization of the engine power at selected points  $(n_s, M_o)$ . A program *Statistica* [30] with 67450 measurement points was used to generate the results.

### 3. Results

The measurements of relative time of engine operation as a function of engine torque and engine speed are presented in Fig. 2, 3 and 4. For better visualization of the relative time of engine operation, the plots for fields A, B and C are normalized to show the measurements within 1% range of  $TD$ .

Two engine operative states were considered: idle and field operation. A quantitative comparison of the time duration of the engine states was ob-

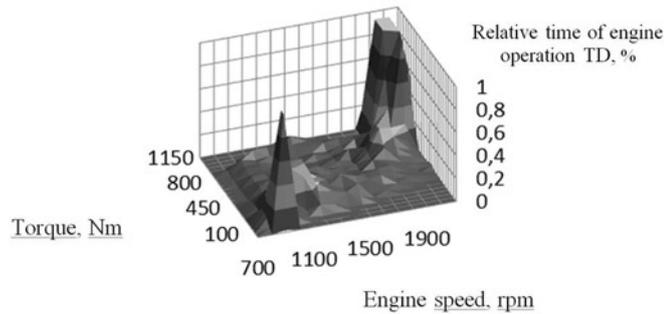


Fig. 2. Relative time of engine operation on field A

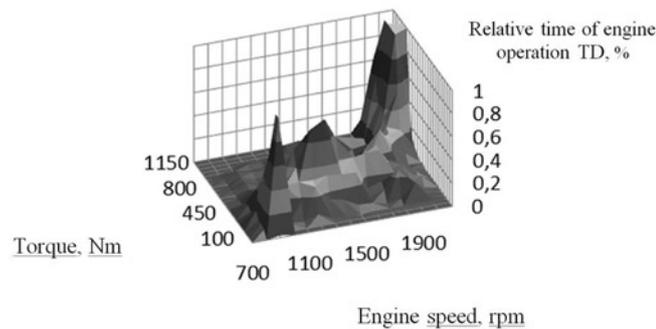


Fig. 3. Relative time of engine operation on field B

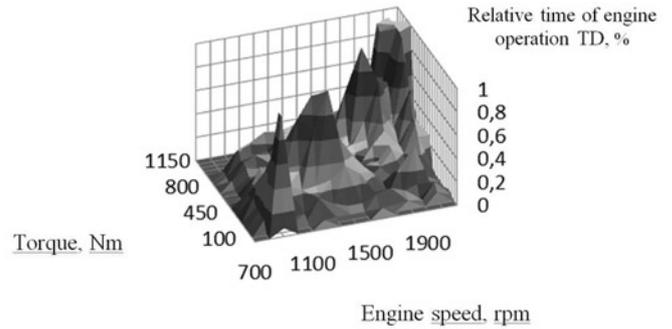


Fig. 4. Relative time of engine operation on field C

tained also using the statistical data clustering approach, with results shown in Fig. 5. Four clusters were obtained as a function of engine speed  $n_s$  and torque  $M_o$ , as well as field size and the corresponding engine state of operation.

For fields A and B, the resulting clusters were comparatively close to each other, as opposed to the cluster locations of field C (Fig. 5). The A and B cluster location coordinates (associated with engine speed and torque) correspond to the engine plowing operation. For clusters variance analysis was performed. It showed strong difference between clusters (Table 3).

Table 3. Variance analysis for the clusters

Effect	Field A		Field B		Field C	
	F	p-Value	F	p-Value	F	p-Value
$n_s$	143565,8	0,00	41483,20	0,00	14324,31	0,00
$M_o$	140147,9	0,00	77110,79	0,00	14324,31	0,00
Number of cases	39833		20535		7082	

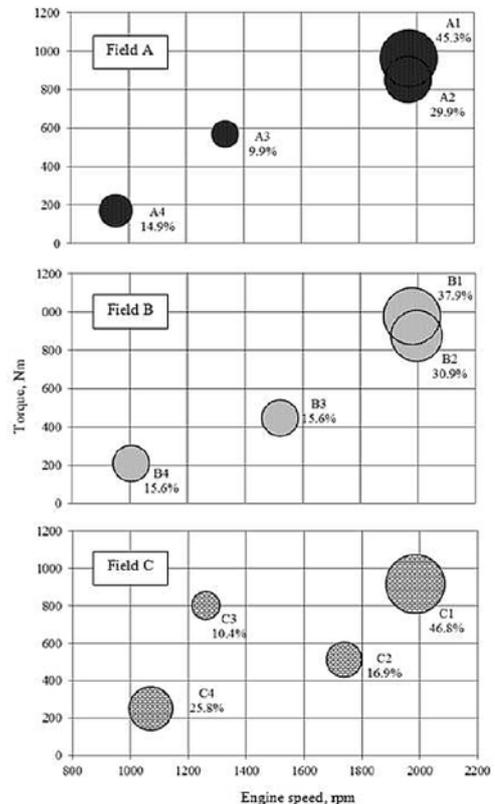


Fig. 5. Engine operation clusters for fields A, B and C; A1, ... C4 – cluster name, % – relative time of engine operation in a cluster

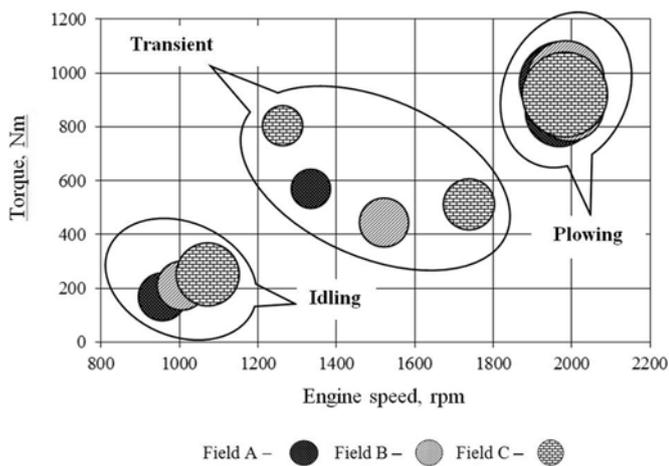


Fig. 6. Engine operational state clusters

During the plowing state interval, the engine was generating 190-195 kW, i.e. about 85% of nominal engine power. For fields A, B and C, the engine was generating 190-195 kW of power 75.2%, 68.8% and 46.8% of total time of engine operation respectively. In the case of engine idling state interval, the corresponding values were 14.9%, 15.6% and 25.8% (Fig. 5). The effective engine utilization  $E_N$  obtained from (3) were accordingly for field A = 0.62, for B = 0.58 and for C = 0.39.

The coordinates of engine for both plowing and idling state intervals for each field clustered within 200 rpm and 100 Nm ranges of engine speed and torque (Fig. 6). The interoperation or transient states spread over 600 rpm and 350 Nm ranges.

A Pearson correlation coefficient was obtained to evaluate the functional relation of plowing vs. idling state share to the field size. Positive correlation (0.92) at  $R^2 = 0,85$  was attained for plowing state and strongly negative ( $-0.85$ ) at  $R^2 = 0,72$  for idling.

#### 4. Discussion

The plowing operations comprise 30% of tractor engine operation while its power is not fully utilized [13, 18]. Continuous monitoring and analysis of economy of agriculture activities contributes to the

#### References

- Chłopek Z. Process modeling of exhaust gas emissions of combustion engine working in traction conditions. *Oficyna Wydawnicza Politechniki Warszawskiej* 1999;173:3-198
- Dyer J. A., Desjardins R. L. Simulated Farm Fieldwork. Energy Consumption and Related Greenhouse Gas Emissions in Canada. *Biosystems Engineering* 2003;85:503-513, [http://dx.doi.org/10.1016/S1537-5110\(03\)00072-2](http://dx.doi.org/10.1016/S1537-5110(03)00072-2).
- Dyer J. A., Desjardins R. L. Carbon Dioxide Emissions Associated with the Manufacturing of Tractors and Farm Machinery in Canada. *Biosystems Engineering* 2006;93:107-118, <http://dx.doi.org/10.1016/j.biosystemseng.2005.09.011>.
- Grisso R., Pitman R. Gear Up and Throttle Down - Saving Fuel. Virginia Cooperative Extension. Virginia Polytechnic Institute and University. Publication 2001;6:442-450.
- Harris H. D. Prediction of the Torque and Optimum Operating Point of Diesel Engines using Engine Speed and Fuel Consumption. *Journal Agricultural Engineering Research* 1992;53:93-101, [http://dx.doi.org/10.1016/0021-8634\(92\)80076-5](http://dx.doi.org/10.1016/0021-8634(92)80076-5).
- Hung W. T., Tong H. Y., Lee C. P., Ha K., Pao L. Y. Development of a practical driving cycle construction methodology: A case study in Hong Kong. *Transportation Research Part* 2007;D12:115-128, <http://dx.doi.org/10.1016/j.trd.2007.01.002>.
- Intex. Fleet Management Systems. [www.intex.net.pl](http://www.intex.net.pl).
- Jahns G., Forster K.J., Hellickson M. Computer Simulation of Diesel Engine Performance. *Transactions of the ASAE* 1990;33:764-770, <http://dx.doi.org/10.13031/2013.31398>.
- Janulevičius A., Juostas A., Pupinis G. Engine performance during tractor operational period. *Energy Conversion and Management* 2013;68:11-19, <http://dx.doi.org/10.1016/j.enconman.2013.01.001>.
- Janulevičius A., Juostas A., Pupinis G. Tractor's engine performance and emission characteristics in the process of ploughing. *Energy Conversion and Management* 2013;75:498-508, <http://dx.doi.org/10.1016/j.enconman.2013.06.052>.
- Kheiralla A. F., Azmi Y., Zohadie M., Ishak W. Modelling of power and energy requirements for tillage implements operating in Serdang sandy clay loam. Malaysia. *Soil and Tillage Research* 2004;78:21-34, <http://dx.doi.org/10.1016/j.still.2003.12.011>.
- Kichler C.M., Fulton J.P., Raper R.L., McDonald T.P., Zech W.C. Effects of transmission gear selection on performance and fuel costs during

minimization of energy usage [25]. Engine torque monitoring represents one of the key parameters in such analysis. Since its measurement requires specialized instrumentation setup, various indirect approaches have been explored [5]. Many such studies have presented their results in a general matrix form and fuel consumption profiles. In the evaluation approach here, performance indexes of operational power performance in various conditions have been presented. Implemented, they can contribute to optimal gear selection through visual display of actual engine power and to "gear up and throttle down" driving approach in transient engine states, possibly resulting in up to 20% fuel savings [4]. The actual engine utilization parameter may also be helpful in optimal tractor selection in terms of cost, as well as match of its engine power to target farm.

Our study, based on a theoretical model of engine optimal points of operation [4], implements a novel statistical data clustering and modern measurement technology approach. The time distributions of engine operation presented here confirm other studies [9, 10] validating our methodological approach. They may also help in modelling agriculture tractor engine load cycles [6], which in turn are used in evaluation of engine emissions.

#### Conclusions:

- The statistical data clustering approach to quantitative comparison of the effective time duration of the various engine modes of operation and fields used in this study enabled more precise evaluation of the actual power utilization of agriculture tractor engine, as a function of field size, than theoretical and simulation approaches.
- The presented statistical approach may have practical applications as an optimization tool in a more effective utilization of various add-on agriculture machinery through a visualization driver support system for optimal gear selection.
- A strong positive correlation was observed between the field size and engine plowing state, while a negative correlation was observed in the case of idling engine state of operation.
- The actual power utilization of agriculture tractor engine as a function of field size was 0.62, 0.58 and 0.39 respectively for the three fields used in this study.

- deep tillage operations. *Soil and Tillage Research* 2011;113:105-111.
13. Kim J.H., Kim K.U., Wu Y.G. Analysis of transmission load of agricultural tractors. *Journal of Terramechanics* 2000;37:113-125, [http://dx.doi.org/10.1016/S0022-4898\(99\)00022-1](http://dx.doi.org/10.1016/S0022-4898(99)00022-1).
  14. Kim Y. J., Chung S. O., Choi C. H. Effects of gear selection of an agricultural tractor on transmission and PTO load during rotary tillage. *Soil and Tillage Research* 2013;134:90-96.
  15. Koniuszy A. The method of making time density characteristic of agricultural tractor engine by using TRS system. *Annual Review of Agriculture Engineering* 2008;6:13-22.
  16. Koniuszy A., Nadolny R., A method and a device of monitoring operation of the tractor. Nr PL 381892;2014.
  17. Kostencki P., Łętkowska B., Nowowiejski R. Field tests of resistance to abrasive wear of ploughshares made of boron steel. *Tribologia* 2013;249:49-79.
  18. Lindgren M. A Transient Fuel Consumption Model for Non-road Mobile Machinery. *Biosystems Engineering* 2005;91:139-147, <http://dx.doi.org/10.1016/j.biosystemseng.2005.03.011>.
  19. Mehta, C. R., Singh K., Selvan M. M. A decision support system for selection of tractor-implement system used on Indian farms. *Journal of Terramechanics* 2011;48:65-73, <http://dx.doi.org/10.1016/j.jterra.2010.05.002>.
  20. Mileusić Z.I., Petrović D.V., Dević M.S. Comparison of tillage systems according to fuel consumption. *Energy* 2010;35:221-228, <http://dx.doi.org/10.1016/j.energy.2009.09.012>.
  21. Moitzi G., Haas M., Wagentristl H., Boxberger J., Gronauer A. Energy consumption in cultivating and ploughing with traction improvement system and consideration of the rear furrow wheel-load in ploughing. *Soil and Tillage Research* 2013;134:56-60.
  22. Pang S.N., Zoerb G.C., Wang G. Tractor Monitor Based on Indirect Fuel Measurement. *Transactions of the ASAE* 1985;28:994-998, <http://dx.doi.org/10.13031/2013.32375>.
  23. Peca J.O., Serrano J.M., Pinheiro A., Carvalho M., Nunes M., Ribeiro L., Santos F. Speed advice for power efficient drawbar work. *Journal of Terramechanics* 2010;47:55-61, <http://dx.doi.org/10.1016/j.jterra.2009.07.003>.
  24. Renius K.T. Trends in Tractor Design with Particular Reference to Europe. *Journal Agricultural Engineering Research* 1994;57:3-22, <http://dx.doi.org/10.1006/jaer.1994.1002>.
  25. Riveiro J. A., Marey-Pérez M. F., Díaz-Varela E. R., Álvarez C. J. A methodology for the analysis of the relationships between farms and their physical environment. *Journal of Agricultural Science* 2010;148:101-116, <http://dx.doi.org/10.1017/S0021859609990347>.
  26. Saglam C., Akdemir B. Annual Usage of Tractors in North-West Turkey. *Biosystems Engineering* 2002;82:39-44, <http://dx.doi.org/10.1006/bioe.2002.0046>.
  27. Sahay C. S., Tewari V. K. Computer Simulation of Tractor Single-point Drawbar Performance. *Biosystems Engineering* 2004;88:419-428, <http://dx.doi.org/10.1016/j.biosystemseng.2004.05.005>.
  28. Serrano J. M., Peca J. O., Pinheiro A., Carvalho M., Nunes M., Ribeiro L., Santos F. The Effect of Gang Angle of Offset Disc Harrows on Soil Tilt. Work Rate and Fuel Consumption. *Biosystems Engineering* 2003;84:171-176, [http://dx.doi.org/10.1016/S1537-5110\(02\)00261-1](http://dx.doi.org/10.1016/S1537-5110(02)00261-1).
  29. Serrano J. M., Peca J. O., Silva M., Pinheiro A., Carvalho M. Tractor energy requirements in disc harrow systems. *Biosystems Engineering* 2007;98:286-296, <http://dx.doi.org/10.1016/j.biosystemseng.2007.08.002>.
  30. Statsoft, Cluster analysis. *Electronic Textbook*, (2015).
  31. Sogaard H. T., Sorensen C. G. A Model for Optimal Selection of Machinery Sizes within the Farm Machinery System. *Biosystems Engineering* 2004;89:13-28, <http://dx.doi.org/10.1016/j.biosystemseng.2004.05.004>.
  32. Souza E.G., Milanez L.F. (1988). Indirect Evaluation of the Torque of Diesel Engines. *Transactions of the ASAE* 1988;31:1350-1354, <http://dx.doi.org/10.13031/2013.30869>.
  33. Souza E.G., Santa Catarina A. Optimum Working Curve for Diesel Engines. *Transactions of the ASAE* 1999;42:559-563, <http://dx.doi.org/10.13031/2013.13216>.
  34. Wang G., Zoerb G.C. Determination of Optimum Working Points for Diesel Engines. *Transactions of the ASAE* 1989;32:1519-1522, <http://dx.doi.org/10.13031/2013.31182>.

**Adam KONIUSZY****Piotr KOSTENCKI**

Department of Systems Engineering Agronomic  
West Pomeranian University of Technology  
al. Piastów 17, 70-310 Szczecin, Poland

**Andrew BERGER**

Physics and Electrical Engineering Department  
University of Scranton  
PA 18510, USA

**Wojciech GOLIMOWSKI**

Department of Biomass Processing Technique  
Institute of Technology and Life Sciences  
ul. Biskupińska 76, 60-463 Poznań, Poland

E-mails: adam.koniuszy@zut.edu.pl, Berger@Scranton.edu,  
w.golimowski@itp.edu.pl